## Multi-Physics Modeling of Doxorubicin Binding to Ion-Exchange Resin in Blood Filtration Devices

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#### Abstract

A group of drugs used in Intra-Arterial Chemotherapy (IAC) have intrinsic ionic properties, which can be used for filtering excessive drugs from blood in order to reduce systemic toxicity. The ion-exchange mechanism is utilized in an endovascular Chemofilter device which can be deployed during the IAC for capturing ionic drugs after they have had their effect on the tumor. In this study, the concentrated solution theory is used to account for the effect of electrochemical forces on the drug transport and adsorption by introducing an effective diffusion coefficient in the advection-diffusion-reaction equation. Consequently, a multi-physics model coupling hemodynamic and electrochemical forces is developed and applied to simulations of the transport and binding of Doxorubicin in the Chemofilter device. A comparison of drug adsorption predicted by the computations to that measured in animal studies demonstrated the benefits of using concentrated solution theory over the Nernst-Plank relations for modeling drug binding.

# MULTI-PHYSICS MODELING OF DOXORUBICINE BINDING TO ION-EXCHANGE RESIN in blood filtration devices

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## Abstract

A group of drugs used in Intra-Arterial Chemotherapy (IAC) have intrinsic ionic properties, which can be used for filtering excessive drugs from blood in order to reduce systemic toxicity. The ion-exchange mechanism is utilized in an endovascular Chemofilter device which can be deployed during the IAC for capturing ionic drugs after they have had their effect on the tumor. In this study, the concentrated solution theory is used to account for the effect of electrochemical forces on the drug transport and adsorption by introducing an effective diffusion coefficient in the advection-diffusion-reaction equation. Consequently, a multi-physics model coupling hemodynamic and electrochemical forces is developed and applied to simulations of the transport and binding of Doxorubicine in the Chemofilter device. A comparison of drug adsorption predicted by the computations to that measured in animal studies demonstrated the benefits of using the concentrated solution theory over the Nernst-Plank relations for modeling drug binding.

## Introduction

Drug transport is one of the key aspects in the design of endovascular devices for drug filtration or elution. Drugs interact with blood and with medical devices through different mechanochemical processes, which depend on their properties. A large group of chemotherapeutic drugs have intrinsic ionic properties; therefore, the ion-exchange mechanisms can be utilized to enhance their effectiveness by reducing adverse side effects. Doxorubicin (Dox) is one of the most commonly used chemotherapeutic drugs used in the Intra-Arterial Chemotherapy (IAC) for treatment of solid tumors, e.g. the primary liver cancer. In the IAC procedure, a cocktail of chemotherapeutic drugs, including Dox, is injected into the arterial blood flow that feeds the tumor. Even though the IAC provides a targeted delivery, less than 50% of drug absorbs to the tumor, while the excessive drug remains in the circulation causing side effects such as an irreversible heart failure <sup>1,2,3</sup>. Dox is positively charged and, therefore, can be filtered from blood by binding to an ionic resin via ion-exchange mechanism in order to reduce systemic toxicity caused by the IAC. A catheter-based Chemofilter device was proposed for eliminating Dox from the venous flow after it has had its effect on the malignant cells of the tumor <sup>1, 4-10</sup>. The Chemofilter deployed during the IAC procedure in veins draining the tumor would adsorb the drug to its surface coated with ionic resin, thus allowing for safer and more efficient treatment.

Significant advances in computational methods have contributed to development of mathematical models which elucidate the underlying mechanisms of convection, diffusion, and reaction. The motivation for this study was to develop a multi-physics modeling approach to analyze transport phenomena in concentrated and dilute electrochemical solutions, as a part of the Chemofilter design project. We present a new method for numerical modeling of drug transport and binding in an electrochemical system as well as the application of this method to simulation of transport and binding of Dox to the Chemofilter device. The modeling results are supported by comparison to measurements reported from animal studies.

A computational model capturing the transport of Dox in the flow and its binding to the ionic surface of the device has to couple the hemodynamic and electrochemical forces. In this study, the mathematical relationships are developed for electrochemical interaction of ionic particles with an ion-exchange surface resulting in a flux of the drug towards the surface. While traditionally the electrochemical force and chemical reaction are represented by a source term in the Navier-Stokes and advection-diffusion-reaction equations, herein the electrochemical body force is embedded in the diffusive term. Consequently, the passive diffusion coefficient is replaced by an effective diffusion coefficient, thus allowing to avoid the source term in the coupled transport equations. Electrochemical systems are typically modelled with the well-established Nernst-Plank equation; however, its application is limited to the dilute solutions. There are few studies of the concentrated solutions, such as that of Dox in blood. In this work, the contribution of electrochemical forces to the coupled Navier-Stokes and Advection-diffusion equations is modelled by using the concentrated solution theory.

In the Theory section of the paper, the relations for the effective diffusion coefficient are developed based on two alternative approaches: the dilute solution theory, and the concentrated solution theory. In the subsequent CFD Modeling section, the obtained relationships are used for numerical simulations of Dox transported through the Chemofilter device. The computational results obtained with each approach are compared to available experimental data.

## Theory

The transport and binding of Dox in the Chemofilter device is affected by a complex interplay of hemodynamic and electrochemical forces. Electrochemical forces are dominant in the electric double layer (EDL), adjacent to the surface and defined as the region where binding of the particles is assumed to be instantaneous. In the EDL, the ion's velocity field may be not divergence-free and is a function of the electrophoretic mobility of ions in the solution. The ion's mobility is, in turn, a function of the electrostatic potential of the electrochemical system which is correlated to the migration of ions<sup>11</sup>. In this study, it was hypothesized that the diffusive and migration terms in the material balance equation could be combined by introducing an effective diffusion coefficient, as described in this section. In the dilute solution approximation, the induced migration of ions was accounted for by using the Nernst-Plank equations<sup>4, 11, 12</sup>, where the solution of Dox in plasma was approximated as 1) a binary solution, and 2) a non-binary solution. In the concentrated solution approximation, the closed form of the effective diffusion coefficient was derived for a binary solution of Dox in plasma. These alternative models for the effective diffusion coefficient are briefly described below.

#### Dilute Solution Theory (Nernst-Plank equation)

In an electrochemical system, the flux density of each dissolved species,  $N_i \text{ [mol/cm}^2\text{]}$ , is due to three transport mechanisms – migration, diffusion, and advection:

$$N_i = -z_i u_i F c_i \nabla \psi_i - D_i \nabla c_i + c_i \mathbf{v}(1)$$

where  $z_i$  is the number of proton charges carried by an ion i,  $u_i$  is the mobility of species i, F is the Faraday's constant,  $c_i$  is the concentration of ion i,  $\psi$  is the electrostatic potential,  $D_i$  is the diffusion coefficient of species i, and  $\mathbf{v}$  is the advective velocity. The material balance for a minor component is formulated as:

$$\frac{\partial c_i}{\partial t} = -\nabla \bullet N_i + \mathcal{R}_i(2)$$

where  $\mathcal{R}_i$  is the reaction (source) term. In the binding of Dox to the ionic resin, the electrochemical force betweenDox<sup>+</sup> and SO<sub>3</sub><sup>-</sup> results in attraction of the particles towards the surface. Assuming a binary electrolyte, the Dox particles in the injected Dox - Cl solution dissociate (Eq. 3) to Dox<sup>+</sup> cations in plasma (solvent) and bind to the surface (Eq. 4), where they form solid species which remain on the surface.

 $Dox - Cl \rightarrow Dox^+ + Cl^-$ (dissociation in solution) (3)

 $\text{Dox}^+ + \text{SO}_3^- \rightarrow Dox - \text{SO}_3(\text{binding of Dox to the surface})$  (4)

By substituting the ion's flux (Eq. 1) to the material balance (Eq. 2) and rearranging the terms, the balance equation for Dox cations reduces to:

$$\frac{\partial c}{\partial t} + \mathbf{v} \bullet \nabla c = D_{\text{eff}} \nabla^2 c + \mathcal{R}(5)$$

where the concentration of the electrolyte is  $c = \frac{c_+}{\nu_+} = \frac{c_-}{\nu_-}$  and  $\nu_+$  and  $\nu_-$  are the number of moles of cations (+) and anions (-) that are produced from dissociation of one mole of the electrolyte (Appendix A). Eq. 5 is the advection-diffusion-reaction equation<sup>11</sup>, with the passive diffusion coefficient replaced by the effective diffusion coefficient:

$$D_{eff-db} = \frac{z_{+}u_{+}D_{-} - z_{-}u_{-}D_{+}}{z_{+}u_{+} - z_{-}u_{-}}(6)$$

where db stands for dilute-binary and the subscripts + and - stand for cation and anion, respectively. The migration term, the first term in Eq. 1, is present when an external potential is applied to the system. In the case of Dox binding to the ionic surface, no external potential is present. Instead, an induced potential term appears in the balance equation due to the electrophoretic mobility of ions. The mobility results in addition of a non-divergence-free term in the velocity,  $\mathbf{v}_{+} = -z_{+}u_{+}F\nabla\psi$ , where  $\mathbf{v} = \mathbf{v}_{0} + \mathbf{v}_{+}$  (see details in Appendix). Therefore, a charge density is induced in the presence of a concentration gradient or a difference of the diffusion coefficients of the anion and cation (note that the diffusion coefficient of Dox is about one order of magnitude lower than that of the other ions such as  $Cl^{-}$  or  $Na^{+}$ ). This charge density creates a non-uniform potential which accelerates the ions with smaller diffusion coefficient towards the surface<sup>11</sup>.

For a non-binary electrolyte, the effective diffusion coefficient was derived for the case where the binding sites were occupied by other ions and the ionic bond on the surface should be overcome before the Dox particles could bind to the surface. This condition was investigated by Schlogl for an electrostatic system,<sup>13, 14</sup> where the exchange of cations from the solution and the resin was considered as:

$$A_s^+ + B_r^+ \to A_r^+ + B_s^+(7)$$

where r denotes resin and s denotes solution. In Schloglet al., <sup>13, 14</sup> the Nernst-Einstein relationship was used to derive the flux of particles as a function of concentration gradient for an electrostatic system (Appendix A). In the current study, Schlogl's model was expanded to model flow dynamics, which results in the material balance equation presented in Eq. 5 with an effective diffusion coefficient expressed as:

$$D_{eff-dnb} = -\frac{2D_A (C_A + C_B)}{\left(\frac{D_A}{D_B} + 1\right)C_A + 2C_B} (8)$$

Where dnb stands for dilute-non-binary, and A and B correspond to  $Dox^+$  and  $Na^+$ . In the new effective diffusion coefficient based on Schlogl binding conditions,  $D_{eff-dnb}$  is a variable which depends on the concentration of the ions.

#### Concentrated Solution Theory

Even though Nernst-Plank equation is widely used in the modeling of electrochemical systems, its application is limited to dilute solutions and its results are based on several other assumptions, such as considering the ions as point charges in order to utilize the Nernst-Einstein relationship <sup>11</sup>. Therefore, in this study, we applied the concentrated solution theory to derive a more generally valid model of the electrochemical binding of Dox to the ionic resin <sup>11, 15</sup>.

In general, there are three main parameters that define the performance of an electrolyte in a concentrated electrochemical system and can be found experimentally; namely the diffusion coefficient, D, the ionic conductivity,  $\kappa$ , and the transference number,  $t_{+}^{0}$ <sup>15, 16</sup>. In the concentrated solution theory, the migration and diffusion is expressed in terms of electrochemical potential as shown in Eq. 9. This equation is analogous to Eq. 1 for dilute solution<sup>11</sup>.

$$c_i \nabla \mu_i = RT \sum_j \frac{c_i c_j}{c_T \mathfrak{D}_{ij}} (\mathbf{v}_j - \mathbf{v}_i) i, \ j = +, -, \ 0 \ (9)$$

Where **v** is the velocity of the species and its subscripts are corresponding to the cations (+), the anions (-),the solution (0), and  $c_T$  is the total concentration ( $\sum_i c_i$ ). In this equation, the interaction of species*i*, *j* is expressed in terms of Stefan-Maxwell diffusion coefficients,  $\mathfrak{D}_{ij}$ , to quantify the relationship between the species velocity, **v**<sub>i</sub>, and the electrochemical potential gradient,  $\nabla \mu_i^{11}$ .

For a binary electrolyte, the flux of the cation and the anion is expressed as:

$$\mathbf{N}_{+} = c_{+}\mathbf{v}_{+} = -\frac{\nu_{+}\mathfrak{D}}{\nu_{\mathrm{RT}}}\frac{c_{T}}{c_{0}}\nabla\mu_{e} + \frac{\mathrm{i}\,t_{+}^{0}}{z_{+}F} + c_{+}\mathbf{v}_{0}(10)$$
$$\mathbf{N}_{-} = c_{-}\mathbf{v}_{-} = -\frac{\nu_{-}\mathfrak{D}}{\nu_{\mathrm{RT}}}\frac{c_{T}}{c_{0}}\nabla\mu_{e} + \frac{\mathrm{i}\,t_{-}^{0}}{z_{-}F} + c_{-}\mathbf{v}_{0}(11)$$

where  $\nu = \nu_+ + \nu_-$  and  $\mu_e = \nu_+ \mu_+ + \nu_- \mu_-$  and the current density is defined as:

$$\mathbf{i} = -\kappa \nabla \psi - \frac{\kappa}{F} \left( \frac{s_i}{n\nu_+} + \frac{\mathbf{t}_+^0}{z_+\nu_+} - \frac{s_0c}{n\mathbf{s}\mathbf{c}_0} \right) \nabla \mu_e$$
(12)

where  $s_i$  is the stoichiometric coefficient of species *i* and *n* is defined as:  $s_+z_+ + s_-z_- = -n$ . It was assumed that the concentration gradient of the anion, Cl<sup>-</sup>, is negligible, since blood plasma already contains a high concentration of Cl<sup>-</sup>, and n = -1. Moreover, the first term on the right- hand-side of Eq. 12 was neglected, as there was no external electric potential in the system; thus, the induced current is defined in terms of  $\nabla \mu_e$ . The gradient of concentration is related to the gradient of electrochemical potential as described by Newman:<sup>11</sup>

$$\frac{\mathfrak{D}}{\nu \operatorname{RT}} \frac{c_T}{c_0} \ c \ \nabla \mu_e = D \left( 1 - \frac{\operatorname{dln} c_0}{\operatorname{dln} c} \right) \nabla c(13)$$

Rearranging the equations, as detailed in the appendix, the material balance equation was finally reduced to:

$$\frac{\partial c}{\partial t} + \nabla \bullet (c\mathbf{v}_0) = \nabla \bullet [D_{eff-cb}\nabla c] + \mathcal{R}(14)$$

where

$$D_{eff-cb} = D\left(1 - \frac{\mathrm{dln}c_0}{\mathrm{dln}c}\right) \left(1 - \frac{\kappa}{z_+F} \left(\frac{s_+}{n\nu_+} + \frac{\mathbf{t}_+^0}{z_+\nu_+} - \frac{s_0c}{n\mathrm{sc}_0}\right) \left(\frac{\nu\mathrm{PT}t_+^0}{2}\right)\right)$$

englishDcc<sub>0</sub> $\frac{1}{c\tau}$ (15)

Eq. 15 provides a closed form expression for the effective diffusion coefficient,  $D_{eff-cb}$ , which includes the effect of induced migration of ions in the concentrated solution, and is expressed as a function of the passive and Stefan-Maxwell diffusion coefficients (D and  $\mathfrak{D}$ ), transference number ( $t^0_+$ ), conductivity ( $\kappa$ ), and concentration of cation and solvent, which are all measurable in experiments.

## **CFD** Modeling

The relationships derived above were used to conduct CFD simulations of Dox transport and binding in the Chemofilter for two alternative configurations of the device. The first configuration, named a Honeycomb Chemofilter (Fig. 1a), consists of parallel hexagonal channels arranged in three separate stages.<sup>9</sup> Detailed CFD modeling of this three-staged design predicted its superior hemodynamic and drug adsorption performance.<sup>9</sup> The other configuration, named a Strutted Chemofilter (Fig. 1b), was used in animal studies,<sup>4</sup> and therefore CFD results for this configuration could be compared to the device filtration measured in vivo. The geometries for both configurations were generated in SolidWorks software and the CAD files were then imported to ANSYS ICEM for numerical mesh generation. The details of discretization, mesh sensitivity analysis, and numerical schemes used in the simulations were described in our previous publications.<sup>8</sup>, <sup>9</sup>

Figure The configuration of (a) 3-stage twisted perforated honeycomb Chemofilter, and (b) single strutted Chemofilter

The coupled Navier-Stokes and Advection-Diffusion-Reaction equations were numerically solved in ANSYS Fluent, to calculate the flow and transport of Dox through the Chemofilter. The Chemofilter device is intended to be deployed in the hepatic veins, therefore the effect of the cardiac pulse can be neglected and the flow was modeled as steady. The flow was also modeled as laminar since the Reynolds numbers in these vessels are less than a hundred. The inlet velocity was set to 0.01 m/s to match the venous flow measured in porcine models, and the outflow boundary condition was assigned to the outlet of the model. In the adsorption of Dox to the Chemofilter, the chemical reaction on the surface was expressed as a sink term to model the elimination of the captured Dox from the system. During the IAC procedure, a steady dose of Dox is injected in the artery for about 10 minutes. In this time interval, it can be assumed that the percentage of Dox that intercalates in tumor cells, as well as the binding capacity of the Chemofilter, i.e. the number of available binding sites, remain constant. In other words, we assume that the mass fraction of Dox at the vein's inlet is constant and the Chemofilter surface does not saturate. Therefore, the steady state conditions were assumed for modeling the Dox injection and transport.

To model Dox binding to the Chemofilter, the energy and species transport modules were activated in Fluent. The chemical reaction was modeled by solving the material balance equation for all species that were introduced in a mixture except the bulk fluid (blood). The chemical reactions were based on Arrhenius model ( $k = A_r T \beta_r e^{-E_r/RT}$ ), where k is the rate constant. A finite rate reaction was chosen for the flow and Arrhenius constants were  $A_r = 1e20$ ,  $\beta_r = 0$ , and  $E_r = 0$ . Mass deposition source was activated to include the effect of surface mass transfer in the continuity equation. The density was calculated based on volume rated mixing law and the diffusivity of Dox in plasma (2.442x10<sup>-10</sup> m<sup>2</sup>/s) was used in the simulations, since the majority of the Dox molecules reside in blood plasma.

Dox mass fraction at the inlet was set to 0.005, and the species site density (of the sulfonate group on the surface) was set to  $10^{-8}$  kgmol/m<sup>2</sup>. It was assumed that the temperature did not change in this process, thus, the energy balance equation was not solved. The diffusion coefficients of chloride anion and sodium cation in blood were set to  $2.032 \times 10^{-9}$ , and  $1.334 \times 10^{-9}$  m<sup>2</sup>/s, respectively.<sup>11</sup> In the simulations based on concentrated solution theory, the electrochemical properties of a high-molecular-weight non-structured polystyrene-*b* - poly(ethylene oxide) (SEO) copolymer electrolyte doped with a lithium salt was utilized<sup>16</sup>, due to the lack of experimental data for Dox performance in plasma. In the species transport module, the effective diffusion coefficient was incorporated into each numerical model with an external User Defined Function (UDF). The UDF was developed in C language and implemented via the species transport dialogue box in Fluent.

## Results

In order to assess the influence of the diffusion coefficient on Chemofilter filtration, numerical simulations of Dox binding to the Honeycomb Chemofilter were conducted with three different diffusion coefficients  $(10^{-10}, 10^{-9}, \text{ and } 10^{-8} \text{ m}^2/\text{s})$ . The simulations were then conducted with the estimated effective diffusion coefficient based on the binary concentrated solution approximation for both Strutted and Honeycomb configurations. Moreover, the simulations with the effective diffusion coefficient derived from dilute solution theory were performed to determine the difference between the results obtained using these two alternative theories. For the dilute solution approximation, the simulations were conducted for both binary and non-binary electrolytes. The mathematical relationships used in the above models are summarized in Table 1.

Table . Computational models considered for Dox binding to the Chemofilter surface

#### Model 1: Filtration based on Passive binding

Figure 2 shows the results of the first study (Table 1), where Dox transport was simulated with different values of the passive diffusivity of Dox particles in plasma. The concentration of Dox decreases as blood flows through each stage of the Honeycomb Chemofilter. The passive diffusion coefficient was set to  $10^{-10}$ ,  $10^{-9}$ , and  $10^{-8} \text{m}^2/\text{s}$ , corresponding to the Peclet number of 50000, 5000, and 500 for the average velocity of 0.01 m/s. The overall Dox mass fraction downstream of the device was predicted to be 0.00476, 0.00373, and 0.00167, corresponding to Dox concentration reduction of 4.7%, 25.4%, and 66.5% for the diffusion coefficients of  $10^{-10}$ ,  $10^{-9}$ ,  $10^{-8} \text{m}^2/\text{s}$ , respectively. The binding predicted in the simulation with diffusion coefficient of  $10^{-8} \text{m}^2/\text{s}$  was the closest match with the binding measured in animal studies, giving the cue that the effective diffusion coefficient must be in the same order of magnitude as the coefficient used in this simulation.

Figure 2 The heat map of Dox concentration changes computed for the Honeycomb Chemofilter using a constant diffusion coefficient of a)  $10^{-10}$  m<sup>2</sup>/s, b)  $10^{-9}$  m<sup>2</sup>/s, and c)  $10^{-8}$  m<sup>2</sup>/s. (In all cases, inlet velocity was 0.01 m/s and inlet Dox mass fraction was 0.005)

#### Model 2: Filtration based on Concentrated Solution Theory

Figures 3a and 3b show a qualitative comparison of the transport and binding of Dox for the Honeycomb and Strutted configurations of the Chemofilter, respectively. This model was based on the concentrated solution theory, which provides a general platform for modeling an electrochemical system. These results were obtained for the effective diffusion coefficient,  $D_{eff}$ , based on the properties of the SEO polymer electrolyte<sup>16</sup>. The calculated effective diffusion coefficient for the SEO polymer electrolyte was about 65 times larger than the passive diffusion coefficient of Dox particles in plasma. The reduction of Dox concentration in blood for the Honeycomb Chemofilter was predicted to be 58.4%. The concentration reduction for the Strutted Chemofilter was predicted to be 43.28%. The computational model slightly underestimated the concentration reduction of 54.1±5%, that was measured in the animal studies. It should be noted that the  $D_{eff}$  was calculated for SEO electrolyte and it is suspected that the effective diffusion coefficient of Dox in blood would be larger than that of SEO copolymer.

#### Model 3: Filtration based on Dilute Solution Theory

The mass fraction of Dox computed for the flow though the three stages of the Honeycomb configuration is shown in Fig 3c. Based on the relations derived for the dilute solution, the effective diffusion coefficient of the binary *Dox-Cl* electrolyte is a constant which depends only on the diffusion coefficients of *Dox* and *Cl*ions in the solution. By using the Nersnt-Einstein relation to express the mobility of ions in term of passive diffusivity, the  $D_{eff-db}$  calculated from Eq. 6 was  $4.128 \times 10^{-10} \text{ m}^2/\text{s}$ . For a non-binary electrolyte, using Schlogl model<sup>13, 14</sup>, the  $D_{eff-dnb}$  was a function of the concentrations of *Dox* and *Na*, as well as their passive diffusion coefficients. The lowest value of  $D_{eff-dnb}$ , 2.44  $\times 10^{-10} \text{ m}^2/\text{s}$ , was found in the near-wall region, where the instantaneous binding results in lower concentration of Dox particles. With the decrease of Dox ions away from the walls and release of Na ions to the solution, the value of  $D_{eff-dnb}$  in the bulk of the flow increased to  $4.36 \times 10^{-10} \text{ m}^2/\text{s}$ .

Figure 3. Mass fraction of Dox computed for the flow through (a) Honeycomb Chemofilter based on concentrated solution theory (b) Strutted Chemofilter based on concentrated solution theory, (c) Honeycomb Chemofilter based on dilute non-binary approximation (Schlogl model), and (d) Percentage of Dox reduction based on different dilute solution models for the Honeycomb and Strutted configuration

The comparison of Dox binding for different Chemofilter configurations with dilute binary and dilute nonbinary approximations is presented in Fig. 3d. Based on the computational predictions for the dilute binary model, the Honeycomb eliminated 13.8% of Dox from the blood stream, while filtration performance decreased to 5.8% for the Strutted configuration. The predicted performance of the Honeycomb and Strutted configurations reduces to 12.2%, and 5.2%, respectively, with dilute non-binary approximation. These results were obtained for the Honeycomb and Strutted configurations with the respective surface area of 4800 mm<sup>2</sup>, and 1900 mm<sup>2</sup>. The pressure drop through the Honeycomb and Strutted Chemofilters were 391 Pa and 288 Pa, respectively.

## Discussion

In this study, a multi-physics computational model for Dox transport and binding to the Chemofilter device was developed. In order to account for the effect of ions migration, the material balance equation was augmented by introducing an effective diffusion coefficient. The modeling was guided by the results of the porcine *in vivo* studies performed at the University of California San Francisco, which are reported in Oh *et al.*<sup>4</sup>. Alternative models of the electrochemical binding of Dox to the Chemofilter surface were developed based on concentrated solution and dilute solution theory. Comparison of the computational results to those reported from the experiments demonstrated the superior performance of the concentrated solution model. In addition, numerical simulations for a range of constant diffusion coefficients were conducted to assess the effect of diffusion coefficient on resulting change in the Dox concentration.

In the animal studies, ion-exchange Chemofilter prototypes with Strutted configuration were deployed in the common iliac vein, and the Dox solution was injected upstream of the device. Analysis of blood aliquots from five samplings locations downstream of the device taken during the 10 minutes of injection showed the removal of  $64\pm6\%$  of Dox from blood plasma, equivalent to  $54.1\pm5\%$  removal from the whole blood<sup>4</sup>. The computational study by Maani *et al.*<sup>9</sup> showed that the Peclet number for Dox transport through the device should be in the order of 500 to match the binding performance observed in the animal studies.

#### Filtration based on Passive Diffusion

The binding of Dox to the Chemofilter was initially simulated using a range of constant diffusion coefficients in order to estimate the order of magnitude of the effective diffusion coefficient which would provide a close match between the computational predictions and experimental measurements. The results presented in Fig. 2a show a marginal filtration performance when the diffusivity of Dox in plasma is used in the material balance equation, thus suggesting that the dominant binding mechanism is due to the electrochemical attraction of the ions towards the surface. The predicted binding performance improves when the diffusion coefficient is increased by two orders of magnitude, demonstrating the closest match to the experiments for the effective diffusion coefficient 100 times larger than the value of the passive diffusion coefficient of Dox in plasma (Fig. 2c).

#### Filtration based on Dilute Solution Theory

The electrochemistry of a dilute electrolyte is well established and expressed with Nernst-Plank equations. Therefore, the binding performance of the Chemofilter was also modeled with the dilute solution approximations for comparison to the concentrated solution model derived herein. Comparing the two dilute solution approximations, the model slightly improved in predicting the binding performance when using binary solution approximation relative to that of the non-binary, as shown in Fig. 3d. The higher performance of the binary solution approximation can be also explained by the fact that for this case there is only one cation (Dox) in the solution and its binding to the anionic surface of the Chemofilter is a one-step reaction. In the non-binary approximation, however, the binding consists of two reactions: the dissociation of sodium from the surface, and reaction of Dox with the surface. The two-step reaction makes the binding process slower as the sodium ions from the surface are being replaced by Dox, which results in lower overall binding performance.

### Comparison of Concentrated and Dilute Solution Theory

Comparing the numerical results obtained utilizing the concentrated and dilute solution models against the experimental data, it can be concluded that the concentrated solution theory provides a more accurate approximation of the binding mechanism than the dilute solution approximations. The reduction of Dox mass fraction in plasma predicted for a non-binary solution shows that the dilute solution approximation severely underestimates the binding of Dox to the Honeycomb Chemofilter (Fig. 3c).

Due to the lack of experimental data on the transport coefficients of Dox-plasma solution, the effective diffusion coefficient formulated in Eq. 15 and implemented in the Chemofilter simulations was based on the SEO polymer electrolyte data<sup>16</sup>. Based on the numbers presented by Villaluenga *et al.*, the effective diffusion of this system was  $1.56 \times 10^{-8} \text{ m}^2/\text{s}$ , which was about 65 times that of the passive diffusion coefficient. The reported salt concentration in the electrolyte<sup>16</sup> was higher than that of Dox in plasma, which magnified the effective diffusion coefficient. However, it can be assumed that migration of Dox particles in plasma is less impeded compared to that in a polymer electrolyte, due to larger mean free path of molecules in blood. As the result, we assumed that the estimated value of the effective diffusion coefficient in a concentrated solution is a function of Dox concentration. Consequently, the effective diffusion coefficient is smaller near the wall, where Dox is being adsorbed to the surface and its concentration is decreasing These results also confirmed the superiority of the Honeycomb design to the Strutted design, as it was predicted by Maani *et al.*<sup>9</sup>.

## Limitations and Future Work

The main limitation in this study was the lack of experimental data characterizing the concentrated solution of Dox in plasma. Thus, the electrochemical characteristics of the SEO polymer electrolyte were utilized in the model. Another simplification of this study is the assumption of a binary electrolyte. In reality, plasma consists of various proteins and ionic components, so Dox molecules may be surrounded or bound to these ionic particles, which affects the mechanism of binding to the filtering surface.

Moreover, in the *in vivo* experiments the geometry and venal flow in the specific animal was not characterized. Therefore, the parameters used in this study were based on the literature and available clinical data. In the *in vivo* studies, two Chemofilter prototypes with 5mm diameter each were deployed in the common iliac vein. However, based on the previous data, we assumed that the filtration performance of two Strutted Chemofilters deployed in parallel is approximately the same as that of one single Strutted Chemofilter with the diameter of 10 mm, which is large enough to fit inside the vein without a gap with the vessel wall where the flow could escape unfiltered.

### Conclusion

A multi-physics modeling approach was developed to investigate the Dox transport and adsorption in the Chemofilter device. The mathematical relationship for an effective diffusion coefficient accounting for ions migration was derived for the concentrated and dilute solution models, and both models were compared to experimental results obtained in animal studies. In the results obtained using the Nernst-Plank equation, the Dox binding performance was underestimated relative to that observed in the experiments. In the models utilizing the concentrated solution theory, the filtration performance predicted by the computational results corresponded to the results of the *in vivo* study. Therefore, we conclude that introducing the effective diffusion coefficient derived from the concentrated solution approximation improves the accuracy of CFD models for Dox transport and binding in the Chemofilter device.

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Conflict of Interest: The authors declare that they have no conflict of interest.

#### References

1. Aboian MS, Yu JF, Gautam A, et al. In vitro clearance of doxorubicin with a DNA-based filtration device designed for intravascular use with intra-arterial chemotherapy. journal article.*Biomedical Microdevices*. October 24 2016;18(6):98. doi:10.1007/s10544-016-0124-5

2. Alexander CM, Maye MM, Dabrowiak JC. DNA-capped nanoparticles designed for doxorubicin drug delivery. *Chem Commun*. 2011;47(12):3418-3420. doi:10.1039/c0cc04916f

3. Alexander CM, Dabrowiak JC, Maye MM. Investigation of the drug binding properties and cytotoxicity of DNA-capped nanoparticles designed as delivery vehicles for the anticancer agents doxorubicin and actinomycin D. *Bioconjugate chemistry* . 2012;23(10):2061. doi:10.1021/bc3002634

4. Oh HJ, Aboian MS, Yi MYJ, et al. 3D Printed Absorber for Capturing Chemotherapy Drugs before They Spread through the Body. ACS Central Science . 2019;5(3):419-427. doi:10.1021/acscentsci.8b00700

5. Kuo W. Binding Kinetics of Cisplatin with Ion-exchange Resins. In: Hetts S, Martin A, Saloner D, VanBrocklin H, editors.: ProQuest Dissertations Publishing; 2016.

6. Maani N, Yee D, Greer JR, Hetts SW, Nosonovsky M, Rayz VL. Computational modeling in design of endovascular Chemofilter device for removing toxins from blood. 2017. p. 1-1.

7. Patel A, Saeed M, Yee E, et al. Development and Validation of Endovascular Chemotherapy Filter Device for Removing High-Dose Doxorubicin: Preclinical Study. J Med Devices . 2014;8(4)doi:10.1115/1.4027444

8. Maani N, Hetts SW, Rayz VL. A two-scale approach for CFD modeling of endovascular Chemofilter device. journal article. *Biomechanics and Modeling in Mechanobiology*. December 01 2018;17(6):1811-1820. doi:10.1007/s10237-018-1058-z

9. Maani N, Diorio TC, Hetts SW, Rayz VL. Computational modeling of drug transport and mixing in the chemofilter device: enhancing the removal of chemotherapeutics from circulation. *Biomechanics and modeling in mechanobiology* . 2020;doi:10.1007/s10237-020-01313-8

10. Yee C, McCoy D, Yu J, et al. Endovascular Ion Exchange Chemofiltration Device Reduces Off-Target Doxorubicin Exposure in a Hepatic Intra-arterial Chemotherapy Model. *Radiology Imaging cancer*. 2019;1(1):e190009. doi:10.1148/rycan.2019190009

11. Newman JS. Electrochemical systems . 3rd ed.. ed. Hoboken, N.J. : Wiley-Interscience; 2004.

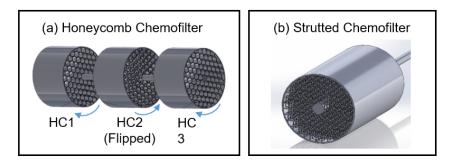
12. Kirby BJ. *Micro- and nanoscale fluid mechanics : transport in microfluidic devices*. New York : Cambridge University Press; 2010.

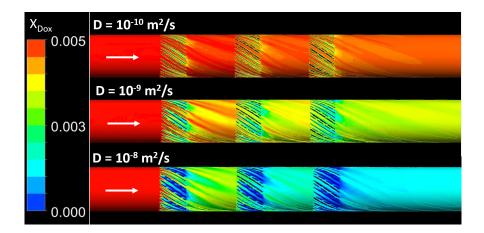
13. Schlögl R, Helfferich F. Comment on the Significance of Diffusion Potentials in Ion Exchange Kinetics. *The Journal of Chemical Physics* . 1957;26(1):5-7. doi:10.1063/1.1743264

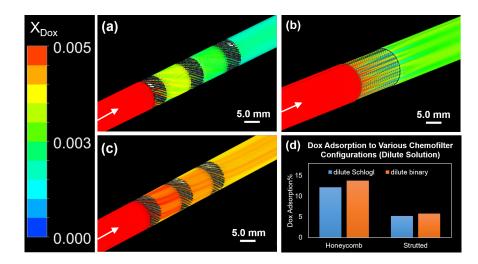
14. Glaski FA, Dranoff JS. Ion exchange kinetics: A comparison of models. *AIChE Journal* . 1963;9(3):426-431. doi:10.1002/aic.690090332

15. Balsara NP, Newman J. Relationship between steady-state current in symmetric cells and transference number of electrolytes comprising univalent and multivalent ions. *Journal of the Electrochemical Society* . 2015;162(14):A2720-A2722. doi:10.1149/2.0651514jes

16. Villaluenga I, Pesko DM, Timachova K, et al. Negative Stefan-Maxwell Diffusion Coefficients and Complete Electrochemical Transport Characterization of Homopolymer and Block Copolymer Electrolytes. *Journal of The Electrochemical Society*. 2018;165(11):A2766-A2773. doi:10.1149/2.0641811jes







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Table 1.docx available at https://authorea.com/users/334786/articles/460720-multi-physics-modeling-of-doxorubicin-binding-to-ion-exchange-resin-in-blood-filtration-devices